

Implementation of Transient Robin Boundary Conditions in OpenFOAM

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Background

The necessity to implement Robin boundary condition (1) arose from formulation of mathematical models of automotive fuses ([1-2],

Fig. 1). Laplacian solver was modified to include source term (heat generated by electric current) and to accept non-linear temperature-dependant physical coefficients.

$$a \frac{\partial T}{\partial n} + bT = \varphi \quad (1)$$

OpenFOAM has pre-defined Dirichlet and Neumann boundary conditions (BC) called *fixedValue* and *fixedGradient* respectively. There is a boundary condition called *mixed*, which is mainly used for switching between the fixed value and the fixed gradient situations on particular boundary, but cannot be used to implement Robin BC directly.

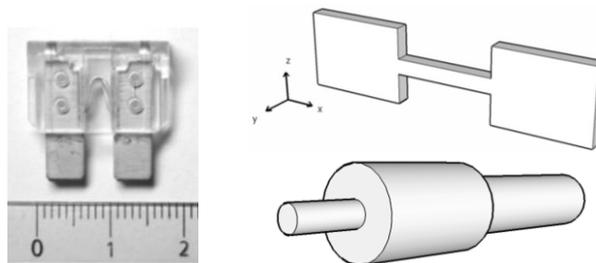


Fig. 1. a) 25A fuse; b) geometry of the Cartesian model; c) geometry of the cylindrical model.

Implementation

Let us consider heat exchange on the surface which is defined as follows:

$$k \frac{\partial T}{\partial n} + \alpha(T - T_\infty) = 0 \quad (2)$$

Here, T is unknown temperature field, k – heat transfer coefficient of solid, α – heat exchange coefficient, T_∞ – ambient temperature, n – face normal. If we compare the formula with the general form (1), $a = k$, $b = \alpha$ and $\varphi = \alpha T_\infty$ are used here.

Let us use *swak4foam* library by B. Gschneider that contains the extension of *mixed* boundary condition called *groovyBC* [3]. By this code, it is possible to define variables and functions on the boundary that are calculated at every internal iteration, and use all available fields and additional pseudo-functions such as *mag* (magnitude) or *delta* (cell-centre to face-centre vector).

We discover from the source code of *mixed* BC how the value on the cell surface is evaluated:

$$T_{face} = f \cdot valueExpr + (1-f)(T_{centre} + gradExpr \cdot \delta),$$

where f is *fractionExpression* defined by user and δ – distance between the cell centre and cell face.

If we linearise the derivative in the formula (2) by T_{face} and T_{centre} , and isolate T_{face} , we obtain:

$$T_{face} = fT_{\infty} + (1-f)T_{center}, \quad f = \left(1 + \frac{k}{\alpha\delta}\right)^{-1}. \quad (3)$$

Comparison with the previous expression shows how to implement this BC in a code.

```

outerSurface
{
    type    groovyBC;
    variables "k=0.2;alpha=15;Tinf=65; f=1/(1+k/(alpha*mag(delta())));";
    valueExpression "Tinf";
    gradientExpression "0";
    fractionExpression "f";
    value    uniform 0;
}

```

Constants k , α and T_{∞} were used here. For the transient parameters, it is recommended to define and calculate them in a solver as fields or calculate directly in *groovyBC*, e.g. “ $k=0.2+0.03*T+4e-5*pow(T,3)$ ”.

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References

Vilums, R., Buikis, A. Conservative Averaging and Finite Difference Methods for Transient Heat Conduction in 3D Fuse. WSEAS Transactions on Heat and Mass Transfer. 3(1):111-124, 2008.

Vilums, R., Liess, H.-D., Buikis, A., Rudevics A. Cylindrical Model of Transient Heat Conduction in Automotive Fuse Using Conservative Averaging Method. The 13th WSEAS Int. Conf. on Applied and Computational Mathematics, Puerto De La Cruz, Tenerife, Spain, 355-360, 2008.

Gschaider, B. Swak4Foam [Online: [http:// openfoamwiki.net/index.php/Contrib/swak4Foam](http://openfoamwiki.net/index.php/Contrib/swak4Foam)]

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